

# Refractive Index Formulae for Radio Waves

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**Key words:** Refractive Index of Air, Radio Waves, Electronic Distance Measurement, Global Positioning System, very long Baseline Interferometry, Microwaves

## ABSTRACT

The radio refractive index formula adopted in 1963 by the International Union of Geodesy and Geophysics (IUGG) and the International Association of Geodesy (IAG) is being reviewed. Forty years ago, this formula was essential for the reduction of distances measured with microwave EDM instruments. Since then, long-range EDM has been replaced by the Global Positioning System (GPS). Today, the formulae are important for accurate measurements using radio waves, including GPS and VLBI (Very Long Baseline Interferometry). The new radio wave refractive index formulae of the last decades are discussed and the inherent problems of some of them are pointed out. State-of-the art formulae for routine and precise measurements in the radio wave spectrum are discussed as are computer programs that model the influences of resonance lines.

Two formulae for hand calculations of the radio refractive index  $N_r$  (in ppm, for infinite wavelengths) have been designed, one based on 'best available' coefficients and one based on 'best average' coefficients. For air with 0.0375% (375 ppm) content of  $\text{CO}_2$ , the latter is:

$$N_r = 77.6890 \frac{p_d}{T} + 71.2952 \frac{p_w}{T} + 375463 \frac{p_w}{T^2}$$

where  $p_d (= p_{\text{tot}} - p_w)$  is the partial dry air (including 375 ppm carbon dioxide) pressure (in hPa),  $p_w$  is the partial water vapour pressure (in hPa), and  $T$  is the temperature (in K). The accuracy of the dry air refractivity component  $N_d$  (first term on right hand side) is, conservatively, 0.02% of  $N_d$ . A conservative value for the accuracy of the water vapour component  $N_w$  (sum of second and third term on the right hand side) is 0.2% of  $N_w$ .

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## 1. INTRODUCTION

The last resolutions of the International Union of Geodesy and Geophysics (IUGG) on refractive indices date back to 1960 and 1963. Because of more recent determinations of the radio wave refractivity of air, the 1960 and 1963 resolutions do no longer satisfy the needs of geodesy and surveying. In consequence, the radio wave formula adopted by IUGG in 1963 is rarely (if ever) used in connection with the GPS (Global Positioning System) and VLBI (Very Long Baseline Interferometry). Even in microwave electronic distance measurement (EDM), the 1963 IUGG resolutions were not universally followed. Although terrestrial microwave distance measurement ( $\lambda = 8 - 30$  mm,  $f = 10 - 35$  GHz) is no longer used on a routine basis in most parts of the world, very long baseline interferometry (VLBI:  $\lambda = 13 - 210$  mm,  $f = 1.4 - 23$  GHz) is, and the Global Positioning System (GPS:  $\lambda = 190 - 250$  mm,  $f = 1.2 - 1.6$  GHz) even more so. A re-evaluation of the radio wave refractive index in geodesy and surveying is, thus, warranted.

In 1991, at the 20th General Assembly of the International Association of Geodesy (IAG) in Vienna, it was suggested that new IUGG resolutions on refractive indices be prepared for adoption at a future General Assembly of IUGG. An ad-hoc working party was formed in due course (Rüeger 1999). Two resolutions on the refractive index of visible and infrared waves were adopted by IAG in 1999 and saw the introduction of a revised default carbon dioxide content of 375 ppm (0.0375 percent). Since then, the review the radio and millimetre wave refractive index has progressed and an interim report has been published recently (Rüeger 2002). Some, but by no means all, key aspects of the interim report (Rüeger 2002) are discussed in this paper.

Unless stated otherwise, the following formula is used for the conversion between the pressure units of mm Hg (or Torr) and hPa (hectopascal):  $p$  [hPa] = (1013.25/760)  $p$  [mm Hg]. The temperature  $T$  (in kelvin, K) is computed from  $T = 273.15 + t$ , where  $t$  is the temperature in degrees Celsius.

## 2. HISTORY OF FORMULAE FOR THE RADIO REFRACTIVE INDEX

The 12th General Assembly of IUGG (Helsinki, 26 July - 6 August 1960) passed a resolution that adopted the following equation (after Essen and Froome 1951) for the reduction of microwave electronic distance measurements (IUGG 1960, Edge 1962):

$$N_r = (n_r - 1) 10^6 = \frac{103.49}{T} (p_{\text{tot}} - p_w) + \frac{86.26}{T} \left(1 + \frac{5748}{T}\right) p_w \quad (1)$$

where  $T$  = temperature (in K),  $p_{\text{tot}}$  = total atmospheric pressure (in mm Hg),  $p_w$  = partial water vapour pressure (in mm Hg),  $n_r$  = refractive index of radio waves in air at ambient conditions,  $N_r$  = refractivity (in ppm) of radio waves in air at ambient conditions. The same

formula was confirmed in another resolution (IUGG 1963) at the 13th General Assembly of IUGG (Berkley, 19 - 31 August 1963). After conversion to hPa (hectopascal) as the pressure unit and into the more common form, the above equation becomes:

$$N_r = (n_r - 1) 10^6 = 77.624 \frac{p_d}{T} + 64.700 \frac{p_w}{T} + 371897 \frac{p_w}{T^2} \quad (2)$$

where  $p_d (= p_{tot} - p_w)$  is the partial pressure of the dry air, the temperature is taken in K and both partial pressures in hPa. The accuracy of Eqs. (1) and (2) was perceived to be  $\pm 0.1$  ppm under 'normal' conditions and better than  $\pm 1.0$  ppm under 'extreme' conditions (Edge 1962). According to Deichl (1984), the simplifications made in the above equation (with respect to the original Essen and Froome equations of 1951) cause systematic errors of about 0.35 ppm (refractive index too small).

As the 1963 IUGG Resolution is based on Essen & Froome (1951), a brief summary of that work is warranted. At 24 GHz, these authors measured the refractive index of dry carbon-dioxide-free air, nitrogen, oxygen, argon and carbon dioxide at mean temperature of 20°C and a mean pressure of 760 mm Hg, and reduced the measurements to 0°C. They measured the refractive index of water vapour in a very limited range of temperatures (15°C and 25°C) and water vapour pressures (8.0 hPa to 18.7 hPa). They give a precision of  $\pm 0.10$  ppm (0.035% of the refractivity value) for their dry air value and of  $\pm 0.1$  ppm (0.165% of the refractivity value) for their water vapour value (at 20°C and 13.3 hPa). They stated that the weak water vapour absorption at 22.23 GHz (13 mm) 'should have an entirely negligible effect' and noted that the water vapour 'extrapolation formula (to other conditions) cannot be given the same confidence as that of the other gases'. Because of their limited temperature range, Essen & Froome (1951) had to predict the  $K_2$  term of the water vapour refractivity from visible values. Hill et al. (1982, p. 1256) noted that Essen & Froome's use of the optical frequency water vapour coefficient  $K_2$  was 'an inaccurate assumption'. Essen & Froome (1951) stated that their simplified equation (Eq. (12), p. 873 of their paper, adopted by IUGG in 1963), introduces errors in refractivity of 0.5 ppm at the extremes of the specified range of temperatures (-20°C, +60°C) and with 'normal' water vapour pressures. (Table 2 shows that, at high temperature and humidity, the simplified Essen & Froome formula differs much more than 0.5 ppm from state-of-the-art formulae.) Their definition of  $T = 273 + t$  introduces further errors. Because of all these deficiencies (of the water vapour terms, mainly), the IUGG formula of 1960 and 1963 should no longer be used.

Since the adoption of the Essen & Froome equation by IUGG in 1960/1963, a great number of investigations into the refractivity of radio and millimetre waves were carried out. The discussion here is restricted to a few contributions that are particularly relevant in the context of geodesy and surveying. For a more complete discussion of the developments in the radio refractive index, readers are referred to Rüeiger (2002).

In 1974, Thayer proposed an 'improved' three-term equation for the radio refractive index for precise geodetic and laboratory use that included compressibility factors. (Although Thayer might have been the first author to use compressibility factors as such for radio refractivity, Essen & Froome (1951, Eq. (11), p. 872) already corrected for the non-ideal gas behaviour in their full equation.) Thayer noted that the omission of compressibility factors leads to errors

in the radio wave refractivity of 0.04 ppm in the dry term and 0.1 ppm in the wet term at high humidities. Thayer (1974) derived his  $K_1$  from the refractivity value published by Smith & Weintraub (1953). The latter obtained their value from a conversion of three published values of the dielectric constant of dry air, one being measured at optical wavelengths and one at 24 GHz. Like Essen & Froome (1951) and, in fact, Thayer himself (1974, before Eq. 6), Hill (1996) points out that the measured radio refractive index is larger than the extrapolated visible one. The accuracy claimed by Thayer (1974) and Smith & Weintraub (1953) is, essentially, that of the optical measurements. (The better of the two microwave measurements is worse by a factor two.) Considering the comments above, Thayer's accuracy claim and the adoption of a partly optical  $K_1$  was inappropriate. Thayer (1974) also 'extrapolated' the 'visible' water vapour refractivity to radio wavelengths and computed the  $K_2$  coefficient from it. He then used Boudouris' (1963) water vapour measurements to derive the  $K_3$  value. Hill (1996) stated that 'the contributions to refraction by water vapour cannot be extrapolated to the infrared and radio regions because of the strong contribution by the infrared resonances of water vapour'. In consequence, the coefficients  $K_1$ ,  $K_2$  and  $K_3$  proposed by Thayer (1974) should **not** be used. Unfortunately, Thayer's coefficients were used later by many authors, particularly in the field of geodesy (e.g. Herring 1992, Jarlemark 1994, Mendes 1999).

Hasegawa & Stokesberry (1975) gave a good summary of 'measured'  $K_1$ ,  $K_2$ , and  $K_3$  values. They computed weighted means for each of the three coefficients, weighting according to the author's standard deviations. Hill et al. (1982) criticised these authors for including the Essen & Froome (1951) and Essen (1953) data because the latter were established over a very limited temperature range. In addition, these authors did not list the frequency at which the experiments were carried out and, thus, ignored the aspect of anomalous refractivity. The authors also ignored the correlation between the  $K_2$  and  $K_3$  terms that degraded some data, including those of Boudouris.

Bevis et al. (1994) revisited the data used by Hasegawa & Stokesberry (1975). They plotted the data, eliminated outliers and computed mean values for  $K_1$ ,  $K_2$  and  $K_3$ . Again, anomalous refractivity was not considered nor the appropriateness of averaging the  $K_2$  and  $K_3$  values separately, considering their high correlation. Like Hasegawa & Stokesberry (1975) before, the authors included the Essen and Froome (1951) and the Essen (1953) data despite the cautionary remarks of Essen & Froome (1951). They also included Barrell's 1951 value that was extrapolated from the visible. In consequence, their standard errors (of the unweighted mean values) of  $\pm 0.05$  k/hPa for  $K_1$ ,  $\pm 2.2$  K/hPa for  $K_2$  and  $\pm 1200$  K<sup>2</sup>/hPa for  $K_3$  should be treated with care.

Mendes (1999) reviewed a number of radio refractivity formula and used them to predict the total delay in distance measurements to GPS satellites. The dry air delays (in zenith direction), computed with the Boudouris (1963, Eq. (3.10) p. 660) and the Smith and Weintraub (1953) formulae (see Mendes, 1999, Table 3.1, p. 59, for coefficients), differ by only 0.6 mm (being 0.026 percent of the dry zenith delay of 2.3 m). Mendes, comparing different water vapour refractivity formulae, found differences smaller than 0.1 mm in the wet zenith delay (Mendes 1999, personal communication). The omission of the compressibility factor for dry air did not change the dry (zenith) delay and that of the compressibility factor

for water vapour did change the wet zenith delay by only 0.1 to 0.2 mm. On the other hand, the omission of the enhancement factor (when computing the water vapour pressure in moist air) changed the wet zenith delay (of 0.258 m) by a maximum of 1.3 mm (at 30° latitude and in summer). Mendes also noted that the wet zenith delay can change by as much as 3 mm, depending on the formula used for the computation of the saturation water vapour pressure. To relate this information to terrestrial measurements, we note that similar dry and wet delays are experienced for a (one-way) horizontal path of 8.58 km length at sea level, 20°C and 28% relative humidity. For low lying satellites (elevation angle of 15°, zenith angle of 75°) the delays are 3.86 times larger (8.9 m for the dry delay and 1.00 m for the wet delay, at 30° latitude and in summer) and the corresponding (one-way) horizontal sea level path length 33.1 km.

### 3. FORMULAE FOR HAND CALCULATIONS (1 HZ TO ABOUT 1 GHZ, M TO 0.3 M)

It is valuable to have a relative simple closed solution for the refractive index of radio waves for easy calculation with pocket calculators and personal computers. The equations given here are empirical, based on experiment and ignore the non-ideal gas behaviour (compressibility) of air. However, some constants have been derived after taking the real gas behaviour into account (e.g. Birnbaum & Chatterjee 1952, and Boudouris 1963). Thayer (1974) stated that omission of the dry air compressibility factor leads to errors of about 0.04 ppm at 500 hPa and that of the water vapour compressibility factor to 0.1 ppm at high humidities. Owens' (1967, p. 55) noted that 'the partial density of CO<sub>2</sub> is always so small that ideal gas behaviour may be assumed' for carbon dioxide. The refractivity  $N_r$  of radio waves can be expressed as:

$$N_r = K_1' \frac{p_{d-c}}{T} + K_2 \frac{p_w}{T} + K_3 \frac{p_w}{T^2} + K_4 \frac{p_c}{T} \quad (3)$$

where  $p_{d-c}$  ( $= p_d - p_c = p_{tot} - p_w - p_c$ ) is the (partial) pressure of the dry carbon-dioxide-free air,  $p_d$  is the (partial) pressure of the dry air ( $= p_{tot} - p_w$ ),  $p_w$  is the partial water vapour pressure and  $p_c$  is the partial carbon dioxide pressure and where the  $K_i$  are constants and  $T$  the temperature.  $K_1'$  is the constant  $K_1$  without the CO<sub>2</sub> component. Because of its polar nature, water vapour has a density ( $K_2$ ) and a density-temperature ( $K_3$ ) term.

#### 3.1 Equation with 'Best Available' Coefficients

After pointing out some erroneous assumption in Thayer's derivations, Hill et al. (1982) supported the use of the coefficients by Boudouris (1963) and Birnbaum & Chatterjee (1952). Following a later suggestion by Hill (1995), the  $K_2$  and  $K_3$  terms are taken from Boudouris (1963) and the  $K_1'$  term (CO<sub>2</sub> free dry air) as well as the carbon dioxide term ( $K_4$ ) from Newell & Baird (1965).

$$K_1' = 77.674 \pm 0.013 \text{ [K/hPa]} \quad (4a)$$

$$K_2 = 71.97 \pm 10.5 \text{ [K/hPa]} \quad (4b)$$

$$K_3 = 375406 \pm 3000 \text{ [K}^2/\text{hPa]} \quad (4c)$$

$$K_4 = 133.484 \pm 0.022 \text{ [K/hPa]} \quad (4d)$$

The precisions listed against  $K_1'$  and  $K_4$  are one half of the  $2\sigma$  values quoted by Newell & Baird (1965). Boudouris (1963) did derive the coefficients  $K_2$  and  $K_3$  from a linear regression solution of his measurements at temperatures from 0°C to +63°C and water vapour pressures from 0 to 127 mm hPa. Measured values for  $K_4$  were also given by Liebe et al. (1977), as  $133.5 \pm 0.15$  K/hPa, and by Zhevakin & Naumov (1967), as  $129.30 \pm 0.02$  K/hPa. Considering that the omission of the CO<sub>2</sub>-term leads to an error of 0.02% only (Hartmann 1993, Hartmann & Leitinger 1984) and that the carbon dioxide content of air is rarely measured by geodesists and surveyors, it is often appropriate to adopt a current value for the CO<sub>2</sub> content and to merge the terms  $K_1'$  and  $K_4$  to give the 'dry-air'  $K_1$  term:

$$K_1 \frac{p_d}{T} = K_1' \frac{p_{d-c}}{T} + K_4 \frac{p_c}{T} = K_1' \frac{p_d - p_c}{T} + K_4 \frac{p_c}{T} = K_1' \frac{p_d}{T} + (K_4 - K_1') \frac{p_c}{T} \quad (5a)$$

Assuming, initially, the traditional 300 ppm (0.03%) content of carbon dioxide,  $p_c$  can be taken as  $0.0003 p_d$ .

$$K_1 \frac{p_d}{T} = \{K_1' + 0.0003 (K_4 - K_1')\} \frac{p_d}{T} = \{77.674 + 0.017\} \frac{p_d}{T} = 77.691 \frac{p_d}{T} \quad (5b)$$

It can be shown that the precision of  $K_1$  is the same as that of  $K_1'$ . The final three-term equation (after Boudouris, Newell and Baird) for air with 0.03% (300 ppm) CO<sub>2</sub> content is:

$$N_r = 77.691 \frac{p_d}{T} + 71.97 \frac{p_w}{T} + 375406 \frac{p_w}{T^2} \quad (6)$$

where the radio refractivity  $N_r$  is in ppm, the dry air (including carbon dioxide) pressure  $p_d$  (=  $p_{\text{tot}} - p_w$ ) and the partial water vapour pressure  $p_w$  are taken in hPa and the temperature  $T$  in K. A comparison of this with other formulae can be found in Tables 1 and 2. Recomputing the  $K_1$  term for a carbon dioxide content of 375 ppm (0.0375%), expected around the year 2004, gives the final form of the formula for the non-dispersive radio wave refractivity  $N_r$  (in ppm, temperature in K and pressures in hPa)

$$N_r = 77.695 \frac{p_d}{T} + 71.97 \frac{p_w}{T} + 375406 \frac{p_w}{T^2} \quad (7)$$

### 3.2 Equation with 'Best Average' Coefficients

Some authors that compiled experimental values of refractivity coefficients did compute mean values of the coefficients for general usage, e.g. Bean (1962), Hasegawa & Stokesberry (1975) and Bevis et al. (1994). The use of 'best average' rather than 'best available' coefficients provides a certain robustness against unmodelled systematic errors and increases the reliability of the values, particularly if data from different laboratories and researchers can be averaged. As an alternative to the formula based on the 'best available' coefficients (see above), the available data have been revisited, and new 'best average' coefficients computed

(Rüeger 2002). Using the newly derived weighted mean coefficients (Rüeger 2002, Tables 4 to 6), the following four-term formula can be constructed:

$$N_r = 77.6681 \frac{P_{d-c}}{T} + 71.2952 \frac{P_w}{T} + 375463 \frac{P_w}{T^2} + 133.4800 \frac{P_c}{T} \quad (8)$$

Using Eq. (5b), the older value of 300 ppm (0.03%) for the content of carbon dioxide and  $p_c$  as 0.0003  $p_d$ , the final three-term equation for the radio refractivity  $N_r$  (in ppm) with weighted mean coefficients for air with 0.03% (300 ppm) content of CO<sub>2</sub> becomes:

$$N_r = 77.6848 \frac{P_d}{T} + 71.2952 \frac{P_w}{T} + 375463 \frac{P_w}{T^2} \quad (9)$$

where the dry air (including carbon dioxide) pressure  $p_d$  ( $= p_{tot} - p_w$ ) and the partial water vapour pressure  $p_w$  are taken in hPa, and the temperature  $T$  in K. The accuracy of the dry air refractivity component  $N_d$  is nominally 0.012% of  $N_d$  or, more conservatively (see Rüeger 2002, Table 2), 0.02% of  $N_d$ . A realistic value for the accuracy of the water vapour component ( $N_w$ ) is about 0.15% of  $N_w$  (Rüeger, 2002, bottom part of Table 5) or, more conservatively (see Rüeger 2002, Table 3), 0.20% of  $N_w$ . A comparison of this with other formulae can be found in Tables 1 and 2. Recomputing the  $K_1$  term for a carbon dioxide content of 375 ppm (0.0375%), expected around the year 2004, gives the final form of the 'weighted mean' formula for the non-dispersive radio wave refractivity  $N_r$  (in units of ppm, K and hPa):

$$N_r = 77.6890 \frac{P_d}{T} + 71.2952 \frac{P_w}{T} + 375463 \frac{P_w}{T^2} \quad (10)$$

#### 4. COMPUTER ROUTINE (1 Hz to about 1 THz, ∞ m to 0.3 mm)

A practical model for the complex refractive index for the propagation calculation of electromagnetic waves through the atmosphere has been developed by Liebe et al. over many years (Liebe 1996 1989 1985, Liebe et al. 1992 1993). The **Millimetre-Wave Propagation Model (MPM)** is as a computer program (for personal (IBM compatible) computers) for frequencies below 1000 GHz in the atmosphere. The MPM 'consists of 44 oxygen and 30 local water resonance lines, of non-resonant spectra for dry air and of an empirical water vapour continuum that reconciles experimental discrepancies' (Liebe et al. 1992). The model is applicable for barometric pressures between 0 and 1200 hPa, ambient temperatures between -100 and +50°C, relative humidity between 0 and 100% and suspended water droplets and ice particle densities between 0 and >5 g/m<sup>3</sup>. The MPM makes use of spectral data and is supported by many laboratory measurements to validate and enhance the overall performance of the model. The authors note that MPM dry-air absorption values agree with measured ones at the 1% level. 'Model predictions involving water vapour and water droplets are estimated to lie in the 10 percent range' (Liebe et al. 1992). Presently, MPM does not provide an input for the CO<sub>2</sub> content. Presumably, a carbon dioxide content of 0.03% is included in the dry-air non-dispersive term. Rüeger (2002, Table 1) has investigated the historical development of the coefficients  $K_1$ ,  $K_2$  and  $K_3$  used by MPM, and their likely origin.

The MPM93 is freely available, fully documented and includes an executable file for IBM PCs as well as the FORTRAN source code. It can be downloaded from the web site of the Institute of Telecommunication Sciences in Boulder, Colorado, USA (<http://www.its.bldrdoc.gov> -> Resources -> Anonymous ftp -> pub/ -> mpm93/ -> refrac/ or directly from <ftp://ftp.its.bldrdoc.gov/pub/mpm93/refrac>). The REFRAC software module is the most useful variant of MPM93 for use in geodesy and surveying. Hill (2000) prepared FORTRAN77 software routines (IR\_N) for the calculation of the phase and group refractive indices of air and its gaseous constituents in connection with a JPL/NASA research project. These subroutines are applicable to wavelengths from the visible through to infinite (radio waves). The effects of absorption resonances of H<sub>2</sub>O, CO<sub>2</sub>, O<sub>2</sub>, O<sub>3</sub>, CH<sub>4</sub>, CO and N<sub>2</sub>O are modelled using the HITRAN data base. The source code can be obtained (on CD) from J. M. Rüeger. It should be noted that there is, presently, no manual for, nor a description of, IR\_N and that some programming by the user is required before IR\_N can be used.

## 5. COMPARISON OF FORMULAE

Tables 1 and 2 show a comparison of the **Millimetre-Wave Propagation Model 1993** (MPM93, non-dispersive refractivity (N<sub>0</sub>) only) with the simple formulae by Essen & Froome (1951, as adopted by IUGG in 1960 and 1963), Boudouris (1963), a formula based on coefficients determined by Liebe et al. (1977), the formula recommended by the International Telecommunication Union in 1986 (CCIR 1986, after Bean & Dutton 1968 and Smith & Weintraub (1952)), a new formula based on the best available coefficients (Eq. (6), after Boudouris (1963) and Newell & Baird (1965)) and a new formula based on the best average coefficients (Eq. 9).

T	PWVP	MPM93	E&F51 IUGG'60 Eq. (2)	Liebe 1977	Boud 1963	Best Available Eq. (6)	Best Average Eq. (9)	CCIR'86
[°C]	$P_w$ [hPa]	$N_r$ [ppm]	$N_r$ [ppm]	$N_r$ [ppm]	$N_r$ [ppm]	$N_r$ [ppm]	$N_r$ [ppm]	$N_r$ [ppm]
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
60	199.26	902.2	892.8	902.2	903.5	903.7	903.4	903.0
45	95.85	597.1	592.2	597.1	597.7	598.0	597.8	597.4
30	42.43	428.3	426.0	428.4	428.5	428.8	428.7	428.3
15	17.04	346.0	345.0	346.1	346.0	346.3	346.3	345.9
0	6.10	314.8	314.3	314.9	314.6	315.0	315.0	314.6
-15	0.00	300.8	300.8	300.9	300.6	301.0	300.9	300.6
-30	0.00	319.3	319.3	319.5	319.1	319.5	319.5	319.1

Table 1: Radio wave refractivity  $N_r$  (in parts per million) computed with the **Millimetre-Wave Propagation Model** and a number of simple formulae at selected temperatures, 1000 hPa total pressure, 300 ppm CO<sub>2</sub> content and 100% relative humidity.

A total pressure ( $p_{tot}$ ) of 1000 hPa exactly was used for the comparison. To be consistent with the historical equations, the Eqs. (6) and (9) for a CO<sub>2</sub> content of 0.03% (300 ppm) were used (rather than Eqs. (7) and (10) for 375 ppm carbon dioxide). The relative humidity was set at 100% for temperatures between 0°C and 60°C. The saturation water vapour pressures used for the computations of Columns 4 to 9 are shown in Column 2 and were taken from



Rüeger (1996, App. B). MPM uses relative humidity as input and converts it to partial water vapour pressure using the equations of Goff & Gratch (1946).

The precision of the new 'best available' formula (Eqs. 6 and 7) was predicted using the propagation law of variances and the given precisions of the constants  $K_1$ ,  $K_2$  and  $K_3$ . Column 10 in Table 2 gives the precision without consideration of the correlation between the constants  $K_2$  and  $K_3$  (correlation coefficient  $\rho = 0.0$ ). Column 11 in Table 2 uses a correlation coefficient of  $-0.995$  between the two constants to compute the covariance between them. This correlation coefficient was obtained from a repetition of Boudouris' curve fit.

T	PWVP	Prec	Prec	(4-3)	(5-3)	(6-3)	(7-3)	(8-3)	(9-3)
	$P_w$	Eq.6	Eq.6	E&F51	Lie77	Bou63	Eq.6	Eq.9	CCIR'86
		$\rho=0.0$		minus	minus	minus	minus	minus	minus
[°C]	[hPa]	[ppm]	[ppm]	[ppm]	[ppm]	[ppm]	[ppm]	[ppm]	[ppm]
(1)	(2)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)
60	199.26	±8.3	±1.2	-9.4	0.0	1.4	1.6	1.3	0.9
45	95.85	±4.2	±0.5	-4.8	0.0	0.6	0.9	0.7	0.3
30	42.43	±2.0	±0.2	-2.3	0.1	0.2	0.5	0.4	0.0
15	17.04	±0.9	±0.1	-1.0	0.1	0.0	0.3	0.3	-0.1
0	6.10	±0.3	±0.0	0.0	0.1	-0.1	0.2	0.2	-0.2
-15	0.00	±0.0	±0.0	0.0	0.1	-0.2	0.2	0.2	-0.2
-30	0.00	±0.0	±0.0	0.0	0.1	-0.2	0.2	0.2	-0.2

Table 2: Comparison of the non-dispersive part of the radio wave refractivity  $N_r$  (in parts per million) from the Millimetre-Wave Propagation Model and a number of simple formulae at selected temperatures, 1000 hPa total pressure, 300 ppm  $CO_2$  content and 100% relative humidity.

Column 12 of Table 2 shows clearly that the Essen & Froome equation (1951) differs significantly from the other three models at high temperature and humidity. Not unexpectedly, the formula ('Liebe77') based on the  $K_1$ ,  $K_2$  and  $K_3$  terms by Liebe et al. (1977) agrees very well with the MPM (see Column 13, Table 2); the differences do not exceed 0.15 ppm between  $-30^\circ C$  and  $+60^\circ C$ . Boudouris' formula agrees slightly better with the MPM93 than Eq. (6) derived above (from the 'best available' coefficients). The differences are, however, smaller than 1 ppm at temperatures below  $50^\circ C$ . Eq. (6) gives values that are, on average, 0.3 ppm higher than those of Boudouris. This is expected since Newell & Baird's  $K_1$  constant is slightly larger than that of Boudouris and since Eq. (6) (see Column 7 in Table 1) uses the same  $K_2$  and  $K_3$  constants as Boudouris' equation (Column 6, Table 1).

The new 'best average' Eq. (9) (see Column 16 in Table 2) shows deviations from MPM93 that are similar to those of Boudouris' equation and Eq. (6). At negative temperatures and zero humidity, the Boudouris' formula and the new Eqs. (6) and (9) have offsets from the MPM93 that are of the same magnitude but different sign. The differences in Columns 14 to 17 of Table 2 compare better with the precision values in Column (11), which take account of the (mathematical) correlation between  $K_2$  and  $K_3$ , than with those in Column (10), which do not. This confirms that the correlation between  $K_2$  and  $K_3$  should not be ignored when predicting the precision of computed refractivity. Columns 14 to 16 in Table 2 further show that the MPM93 seems to underestimate the radio refractive index at high humidities and high temperatures when compared to the four alternative formulae tabled.

## 6. CONCLUSIONS

The radio refractive index formula recommended in Resolution No. 1 of the 13th General Assembly of IUGG (Berkley 1963) is now clearly out of date. With new absolute and relative measurements of the mid-infrared to radio wave refractive index of air being available, and with considerable advances having been made with the computation of anomalous refractivity in the mid-infrared to radio wave spectrum, there is a clear need to rescind the 1963 IUGG resolutions and to propose a more appropriate alternative.

Since a number of authors, particularly in the field of geodesy (e.g. Herring 1992, Jarlemark 1994, Mendes 1999), have started using the radio refractive index formula and coefficients of Thayer (1974), it is stressed again that the coefficients  $K_1$ ,  $K_2$  and  $K_3$  proposed by Thayer (1974) should **not** be used. As explained before, Thayer's  $K_1$  and  $K_2$  have been derived, at least in part, from optical data, which is inappropriate.

No final proposal for a 'best' simple formula for hand calculations is presented. If the MPM is taken as reference, then a formula of the type of Eq. (10), with the constants  $K_1$ ,  $K_2$  and  $K_3$  determined by Liebe et al. (1977), produces the best agreement. On the other hand, if the newly derived 'best available' and 'best average' formulae (see Eqs. 7 and 10) are taken as reference, then the MPM needs some fine tuning. The relative merits of the  $K_2$  and  $K_3$  values by Boudouris (1963) and Liebe et al. (1977) as well as of the  $K_1$  values by Newell & Baird (1965) and Liebe et al. (1977) need to be established before a final decision on an appropriate course of action can be made.

For frequencies above 1 GHz and, particularly, for frequencies close and beyond the relevant resonance lines (e.g. between 53.59 and 66.30 GHz and at 118.75 GHz for oxygen, at 22.23 GHz, 67.81 GHz and 119.99 GHz for water vapour) anomalous refractivity has to be modelled. Liebe's Millimetre-Wave Propagation Model (MPM) for frequencies below 1000 GHz is, presently, the most accessible computer routine that models anomalous refractivity of oxygen and water vapour. Hill's software routines (IR\_N) use a much more complete set of resonance lines (HITRAN), but require some FORTRAN programming by the user.

It is shown in Rüeger (2002) that the most meaningful precision information is quoted in percent of the refractivity  $N_i$  or in percent of the refractivity coefficient  $K_i$ . Rüeger (2002) used a relative precision of  $\pm 0.02\%$  for the dry air refractivity ( $N_d$ ) and of  $\pm 0.2\%$  for the water vapour refractivity ( $N_w$ ) and considers these values realistic and, possibly, somewhat conservative. Readers requiring an in-depth review of the radio refractive index should refer to Rüeger (2002) which gives much more information than the technical paper at hand. Rüeger (2002) comes bundled with earlier reports on the refractive index of air.

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