# Geodetic Measurements for Detecting Movements on the Structure Surface Due to Mining Activities

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#### INTRODUCTION

Mining activities cause to create gaps inside the ground. The gaps withstand the load over it by vaulting inside the ground and prevent caving-in as long as they are opened deeper into ground and remain in smaller proportions as is the case in mining galleries depending upon the production length.

With the mining production gaps reaching larger dimensions, however, the ground just above the gaps starts to collapse by layers breaking away and fills up the production gaps.



The movements of ground on the surface triggered by the collapse of cascading internal ground layers are termed as mining subsidence (Kratzsch, 1983; Kuşçu,1991; Perski and Jura, 2003; Deck *et al.*, 2003; Duzgun, 2005; Akçın *et al*, 2006; Saeidi *et al.*, 2009; Can *et al.*, 2011a, 2011b).

These movements cause deformations on the earth surface and in the affected ground layers and disruptions on the natural balance of ground. As a consequence of this, engineering structures inside the affected ground and on the earth surface above the subsidence region either accommodate to these deformations or sustain damages These damages whether they occur on natural or man-made structures by means of mining subsidence are called mining damages.

In Zonguldak Kozlu Hard Coal Region, coal seams dip mostly at high angle and their thicknesses are not uniform, therefore mining subsidence problems are most likely to occur causing very serious problems with regard to urbanization.

#### 2. MONITORING OF MINING SUBSIDENCE

It is necessary to gather information on general and regional properties of subsidence formation and effective constituents which eventually cause damages on structures in order to mitigate mining subsidence induced issues and to provide solutions.

Therefore it is of great importance that subsidence measurements and observation should be conducted on the earth surface and, if necessary, in the underground.

Even though the mining activities have been going on for 160 years in Zonguldak Hard Coal Basin there exists little or no knowledge on this, which is needed dearly today especially with the densification of settlement areas just above the old coal production galleries and mining activities continuing under new settlement areas.

The coal seams in Kozlu production region have steep inclinations as is generally the case in Zonguldak Hard Coal Basin and the subsidence occurring in this region have adverse effects on social, economic and legal aspects of life (Turer, 2008).



Figure 2. Subsidence tub forming after production in inclined coal seams and the other related definitions (Kratzsch, 1983).

Fig 2 depicts the subsidence formation and its influence areas after mining activities in inclined coal seams in the region.



In order to determine the subsidence occurring due to mining activities in an underground mine production region, subsidence measurements are utilized to ascertain:

- •Subsidence parameters (critical and limit angles, displacement values etc.),
- •Relationship between subsidence and geology, tectonics and topography,
- •Relationship between subsidence and production speed and time,
- •Relationship between subsidence and production method,

# 3. FEATURES OF KOZLU COAL PRODUCTION REGION

Kozlu-Zonguldak Hard Coal Basin is a formation of the Late Plaeozoic–Mesozoic Age, consisting of various faults and topographic irregularities along the North Anatolian Mountain Range.

The town of Kozlu within the Zonguldak Hard Coal Basin was established in 1941 and has a coal production rate of 780,000 ton per year along with 3.3 million ton per year in the whole basin (URL1 2011; URL 2 2011).







Fig 5b Kozlu Seaport (Study Area) in the Kozlu coal production region

### 4. GEOMETRICAL PROPERTIES OF MINING PANELS AFFECTING KOZLU SEAPORT

The coal seams under the engineering structures focused on in this study have steep inclination angles, and they house production panels working on longwall method. Figures 6 demonstrate Ikonos satellite images containing old and new production panels just under Kozlu Seaport with active and residual subsidence effects.



Figure 6 Influence areas of old and new production panels in Kozlu Seaport under active and residual subsidence influences.

able 1a. Geometrical properties of production panel							
nder Kozlu Seaport (computed in accordance with the National Co							
bard (NCB))							
Panel name	Year	Inclination	Thickness	Width	H <sub>mean</sub>		
E.U.2 (old)	1988	40°	3m	60m	-456m		
E.U.3 (old)	1990	40°	3m	60m	-434m		
E.U.4 (old)	2004	58°	3m	50m	-510m		
E.U.5 (old)	2006	32°	2m	110m	-508m		
E.U.6 (old)	1989	26º	1.5m	190m	-400m		
E.U. 10 (old)	1987	28°	3m	120m	-283m		
E.U.12 (old)	1990	27°	3m	80m	-256m		
E.U.13 (old)	1990	17°	3m	60m	-321m		
Y.U.2 (new)	2009	29°	2.5m	130m	-510m		
Y.U.3 (new)	2009	20°	2m	30m	-445m		
Y.U.4(new)	2009	44°	2m	20m	-450m		
Y.U: New mining	g panels	E.U: Old minin	g panels				

Table 1b.The maximum possible subsidencemagnitudes and parameters computed in accordancewith the NCB in Kozlu Seaport region.

Panel name	S <sub>max</sub> (vertical)	Subsidence type	$\gamma_{lower}$	γ <sub>medium</sub>	$\gamma_{upper}$
E.U.2 (old)	0.4cm	Residual	28°	55°	85°
E.U.3 (old)	0.2cm	Residual	28°	55°	85°
E.U.4 (old)	1.1cm	Residual	29º	55°	84º
E.U.5 (old)	1.3cm	Residual	29º	55°	83°
E.U.6 (old)	9.5cm	Residual	32°	55°	81º
E.U. 10 (old)	1.9cm	Residual	30°	55°	83°
E.U.12 (old)	5.9cm	Residual	30°	55°	82º
E.U.13 (old)	0.6cm	Residual	38°	55°	75°
<b>Y.U.2 (new)</b>	3cm	Active	30°	55°	82°
Y.U.3 (new)	1cm	Active	37º	55°	76°
Y.U.4(new)	0.3cm	Active	27º	55°	85°

Table 3a lists the computed semi-major and –minor axes values of an ellipse enveloping possible subsidence affected areas of old and new production panels in Kozlu Seaport under residual and active subsidence effects for plotting purposes

Panel name	Semi-major and -minor axes of subsidence influence areas				
	a(m)	b(m)	Area (km <sup>2</sup> )		
E.U.2 (old)	1002m	748m	0.59 km <sup>2</sup>		
E.U.3 (old)	961m	668m	0.50 km <sup>2</sup>		
E.U.4 (old)	1091m	994m	0.85 km <sup>2</sup>		
E.U.5 (old)	1147m	870m	0.78 km <sup>2</sup>		
E.U.6 (old)	1052m	750m	0.62 km <sup>2</sup>		
E.U. 10 (old)	693m	476m	0.26 km <sup>2</sup>		
E.U.12 (old)	591m	588m	0.27 km <sup>2</sup>		
E.U.13 (old)	565m	558m	0.24 km <sup>2</sup>		
Y.U.2 (new)	1142m	784m	0.70 km <sup>2</sup>		
Y.U.3 (new)	736m	652m	0.38 km <sup>2</sup>		
Y.U.4(new)	959m	720m	0.54 km <sup>2</sup>		

#### 5. PRECISE LEVELING AND GPS MEASUREMENTS IN KOZLU SEAPORT

In order to determine subsidence magnitudes in the aforementioned region just under the engineering structures three periods of precise leveling and GPS measurements were conducted in August 2009, May 2010 and November 2010.

The one hour static GPS data were collected at the subsidence monitoring points with an observation epoch of 2009.58 in the first period, 2010.40 in the second period and 2010.90 in the third period.

Table 4 a,b,c lists horizontal displacement vectors of subsidence monitoring points T34, T35, T36, T37, T38, T39 and T40 in Kozlu Seaport.

	DIFFERENCES BETWEEN PERIODS I AND II (August 2009-May 2010)							
Point #	Point # Point # Y (Easting) X (Northing) Horizontal Disp. RMSE (±) (n							
4.0		(m)	(m)	Vector (m)				
4d T.34	T.34	-0.063	0.014	0.065	0.0042			
T.35	T.35	-0.069	0.008	0.070	0.0045			
T.36	T.36	-0.056	-0.013	0.058	0.0058			
T.37	T.37	-0.051	0.005	0.051	0.0063			
T.38	T.38	-0.070	0.027	0.075	0.0037			
T.39	T.39	-0.068	0.037	0.077	0.0036			
T.40	T.40	-0.073	0.051	0.089	0.0054			
DIFFERENCES RETWEEN DERIODS II AND III (May 2010 November 2010)								
Point #	Point #	V (Fasting)	X (Northing)	Horizontal Disn	RMSE (+) (m)			
1 omen	1 one //	(m)	(m)	Vector (m)	10110L (=) (III)			
T.34	T.34	-0.021	0.012	0.024	0.0040			
T.35	T.35	-0.016	0.025	0.029	0.0031			
T.36	T.36	-0.022	-0.004	0.022	0.0037			
T.37	T.37	-0.028	0.004	0.029	0.0028			
T.38	T.38	-0.017	0.002	0.017	0.0036			
	T.39	-0.017	0.028	0.033	0.0035			
T.39								
T.39 T.40	T.40	-0.051	0.039	0.064	0.0034			
T.39 T.40 DIFFEF	T.40 ENCES BET	-0.051	0.039 IODS I AND II	0.064 I (August 2009-Nov	0.0034 ember 2010)			
T.39 T.40 DIFFEF Point #	T.40 ENCES BET Point #	-0.051 WEEN PER Y (Easting)	0.039 IODS I AND II X (Northing)	0.064 I (August 2009-Nov Horizontal Disp.	0.0034 ember 2010) RMSE (±) (m)			
T.39 T.40 DIFFER Point #	T.40 ENCES BET Point #	-0.051 WEEN PER Y (Easting) (m)	0.039 IODS I AND II X (Northing) (m)	0.064 I (August 2009-Nov Horizontal Disp. Vector (m)	0.0034 ember 2010) RMSE (±) (m)			
T.39 T.40 DIFFEF Point # T.34	T.40 ENCES BET Point # T.34	-0.051 WEEN PER Y (Easting) (m) -0.085	0.039 IODS I AND II X (Northing) (m) 0.026	0.064 I (August 2009-Nov Horizontal Disp. Vector (m) 0.089	0.0034 ember 2010) RMSE (±) (m) 0.0043			
T.39 T.40 DIFFEE Point # T.34 T.35	T.40 ENCES BET Point # T.34 T.35	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033	0.064 I (August 2009-Nov Horizontal Disp. Vector (m) 0.089 0.091	0.0034 ember 2010) RMSE (±) (m) 0.0043 0.0050			
T.39 T.40 DIFFEE Point # T.34 T.35 T.36	T.40 ENCES BET Point # T.34 T.35 T.36	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085 -0.085 -0.078	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033 -0.017	0.064 I (August 2009-Nov Horizontal Disp. Vector (m) 0.089 0.091 0.080	0.0034 mber 2010) RMSE (±) (m) 0.0043 0.0050 0.0054			
T.39   T.40   DIFFEF   Point #   T.34   T.35   T.36   T.37	T.40 ENCES BET Point # T.34 T.35 T.36 T.37	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085 -0.078 -0.080	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033 -0.017 0.009	0.064 I (August 2009-Novi Horizontal Disp. Vector (m) 0.089 0.091 0.080 0.080	0.0034 mber 2010) RMSE (±) (m) 0.0043 0.0050 0.0054 0.0063			
T.39   T.40   DIFFEF   Point #   T.34   T.35   T.36   T.37   T.38	T.40 ENCES BET Point # T.34 T.35 T.36 T.37 T.38	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085 -0.078 -0.080 -0.087	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033 -0.017 0.009 0.029	0.064 I (August 2009-Novi Horizontal Disp. Vector (m) 0.089 0.091 0.080 0.080 0.080	0.0034 mber 2010) RMSE (±) (m) 0.0043 0.0050 0.0054 0.0063 0.0043			
T.39 T.40 DIFFEE Point # T.34 T.35 T.36 T.37 T.38 T.39	T.40 ENCES BET Point # T.34 T.35 T.36 T.37 T.38 T.39	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085 -0.080 -0.087 -0.085	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033 -0.017 0.009 0.029 0.065	0.064 I (August 2009-Nove Horizontal Disp. Vector (m) 0.089 0.091 0.080 0.080 0.092 0.107	0.0034 ember 2010) RMSE (±) (m) 0.0043 0.0050 0.0054 0.0063 0.0043 0.0039			
T.39 T.40 DIFFEE Point # T.34 T.35 T.36 T.37 T.38 T.39 T.40	T.40 ENCES BE T.34 T.35 T.36 T.37 T.38 T.39 T.40	-0.051 WEEN PER Y (Easting) (m) -0.085 -0.085 -0.087 -0.085 -0.124	0.039 <b>IODS I AND II</b> <b>X (Northing)</b> (m) 0.026 0.033 -0.017 0.009 0.029 0.065 0.089	0.064 I (August 2009-Nove Horizontal Disp. Vector (m) 0.089 0.091 0.080 0.080 0.092 0.107 0.153	0.0034 ember 2010) RMSE (±) (m) 0.0043 0.0050 0.0054 0.0063 0.0043 0.0039 0.0052			

Figures 4 depict Ikonos satellite images containing horizontal displacement vectors obtained using the three periods of GPS measurements on the subsidence monitoring points in Kozlu Seaport.

![](_page_10_Figure_3.jpeg)

It is hard to imply that horizontal and vertical displacements have caused any visual deformations or functional defects in the seaport during the three periods of GPS and precise leveling measurements in the region.

As for the vertical displacements Tables 5 list the findings obtained from the three period pairs of precise leveling measurements for Kozlu Seaport

Table 5. Vertical displacement vectors of subsidence monitoring points in Kozlu Seaport with their RMSE values for the period pairs

	Vertical Displacements (m)							
	Period pair		Period pair		Period pair I-III			
	I-II	RMSE	II-III	RMSE	(Aug 09-Nov 10)	RMSE		
	(Aug 09-	(m)	(May 10-Nov	(m)		(m)		
Point #	May 10)		10)					
T34	-0.067	0.003	-0.027	0.003	-0.094	0.004		
T35	-0.065	0.003	-0.026	0.003	-0.091	0.004		
T36	-0.045	0.003	-0.020	0.003	-0.065	0.004		
<b>T37</b>	-0.042	0.003	-0.019	0.003	-0.061	0.004		
T38	-0.045	0.003	-0.015	0.003	-0.060	0.004		
T39	-0.045	0.003	-0.019	0.003	-0.064	0.004		
T40	-0.066	0.003	-0.031	0.003	-0.097	0.004		

Figures 5 depicts Ikonos satellite images containing vertical displacement vectors obtained using the three periods of precise leveling measurements on the subsidence monitoring points in Kozlu Seaport

![](_page_12_Figure_2.jpeg)

#### **6.CONCLUSIONS**

Kozlu mining production region with extensive mining activities houses, many crucial engineering structures such as Kozlu Seaport which are the core of this study and there are plans for new constructions on even daily basis in the region.

In order to maintain the mining operations along with urban developments in a healthy way, the subsidence monitoring measurements and observations play important role in mitigating or even preventing the damages that possibly will occur in future and in giving way to desired urban development in the region

#### In the study

• It has been determined that the horizontal displacements in Kozlu Seaport vary from 8.0cm to 15.3cm with their rmse values of 3.9mm to 6.3mm, respectively, obtained from the GPS measurements between the periods of I (Aug 2009) and III (Nov 2010).

• On the other hand, the vertical displacements obtained from the three periods of precise leveling measurements have been found to deviate from 6.0cm to 9.7cm in the seaport region with 3.0 and 4.0mm rmse values.

#### Since the mining operations under Kozlu Seaport and will also be active in future, in the lights of findings obtained from this study it is suggested that an extensive subsidence monitoring measurements with longer periods should be carried out to mitigate and even prevent functional problems that may arise in these engineering structures in future.

## THANKS FOR YOUR ATENTION

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